

THE CALCULATION OF THE THERMAL STRESSES IN A
CYLINDER AND A SPHERE WITH VARIABLE
SURFACE TEMPERATURE

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The calculation of the thermal stresses at the surface and at the center of a cylinder and a sphere is suggested to be carried out with the use of the integral-mean temperature and the temperature of the center, computed through the multiplication of a piecewise-linear approximating surface temperature by specific coefficients.

For the determination of the thermal stresses in a cylinder and a sphere it is necessary to know the distribution of the temperature over the cross section [1]:

$$\left. \begin{aligned} \sigma_r &= \frac{1}{2} \frac{\alpha E}{1-\nu} [\bar{t}(1) - \bar{t}(\bar{r})] \text{ --- is the stress in the radial direction} \\ \sigma_\tau &= \frac{\alpha E}{1-\nu} \left[\frac{1}{2} \bar{t}(1) + \frac{1}{2} \bar{t}(\bar{r}) - t(\bar{r}) \right] \text{ --- is the stress in the tangential} \\ &\hspace{15em} \text{direction,} \\ \sigma_z &= \frac{\alpha E}{1-\nu} [\bar{t}(1) - t(\bar{r})] \text{ --- is the stress in the axial direction of the} \\ &\hspace{15em} \text{cylinder,} \end{aligned} \right\} \quad (1)$$

and

$$\left. \begin{aligned} \sigma_r &= \frac{2}{3} \frac{\alpha E}{1-\nu} [\bar{t}(1) - t(\bar{r})] \text{ --- is the stress in the radial direction} \\ \sigma_\tau &= \frac{\alpha E}{1-\nu} \left[\frac{2}{3} \bar{t}(1) + \frac{1}{3} \bar{t}(\bar{r}) - t(\bar{r}) \right] \text{ --- is the stress in the tangential} \\ &\hspace{15em} \text{direction of the sphere.} \end{aligned} \right\}$$

The problem of the determination of the heating of a cylinder and a sphere, under a surface temperature which varies in time, can be solved numerically by the method of elementary balances. The subsequent determination of the stresses is also connected with numerical computations. Because of the great labor-consuming character of such computations, we make an attempt to develop a method of calculation of the thermal stresses which allows us, omitting the computation of the temperature field, to find at once the variation of the integral-mean temperature and the temperature at the considered point of the cylinder or sphere, necessary for the determination of the stresses as a function of the variation of the surface temperature.

It is known that if the surface temperature of the cylinder or the sphere varies step-wise from the initial uniform temperature (equal to zero in our case) to some constant value, then the temperature field over the cross section of the cylinder and the sphere is determined by the formula [2]

$$t = t_w \left(1 - \sum_{n=1}^{\infty} A_n e^{-\mu_n^2 Fo} \right), \quad (2)$$

where

$$A_n = \frac{2}{\mu_n} \frac{J_0(\mu_n \bar{r})}{J_1(\mu_n)}; \quad \mu_n \text{ --- are the roots of the function } J_0, \text{ for the cylinder,}$$

$$A_n = 2(-1)^{n+1} \frac{\sin \mu_n \bar{r}}{\mu_n \bar{r}}; \quad \mu_n = n\pi \text{ --- for the sphere}$$

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TABLE 2. The Variation of the Coefficients B_{i-m} for the Integral-Mean Temperature of the Cylinder as a Function of the Computation Interval ΔFo and the Parameter $(i-m)$

$i-m$	ΔFo																			
	0,01	0,02	0,03	0,04	0,05	0,06	0,07	0,08	0,09	0,10	0,12	0,14	0,16	0,18	0,20	0,3	0,4	0,6	0,8	1,0
0	0,1455	0,2026	0,2452	0,2803	0,3105	0,3373	0,3614	0,3835	0,4039	0,4228	0,4572	0,4877	0,5153	0,5402	0,5631	0,6536	0,7171	0,7978	0,8452	0,8753
1	0,1142	0,1552	0,1841	0,2065	0,2246	0,2400	0,2526	0,2635	0,2728	0,2816	0,2927	0,3009	0,3056	0,3079	0,3079	0,2885	0,2563	0,1962	0,1533	0,1243
2	0,0707	0,0933	0,1079	0,1178	0,1248	0,1291	0,1329	0,1360	0,1377	0,1312	0,1255	0,1175	0,1082	0,0982	0,0884	0,0478	0,0239	0,0058	0,0014	0,0004
3	0,0550	0,0710	0,0799	0,0850	0,0871	0,0868	0,0850	0,0816	0,0774	0,0727	0,0623	0,0521	0,0427	0,0346	0,0278	0,0084	0,0024	0,0001	0	0
4	0,0459	0,0579	0,0635	0,0650	0,0648	0,0608	0,0562	0,0514	0,0459	0,0406	0,0311	0,0231	0,0170	0,0122	0,0087	0,0014	0,0002	0	0	0
5	0,0398	0,0489	0,0519	0,0509	0,0475	0,0428	0,0375	0,0320	0,0273	0,0228	0,0156	0,0103	0,0067	0,0043	0,0027	0,0003	0	0	0	0
6	0,0352	0,0421	0,0430	0,0403	0,0355	0,0303	0,0250	0,0202	0,0162	0,0128	0,0078	0,0050	0,0026	0,0015	0,0010	0,0001	0	0	0	0
7	0,0317	0,0368	0,0359	0,0321	0,0265	0,0213	0,0167	0,0128	0,0096	0,0071	0,0039	0,0020	0,0012	0,0006	0,0002	0	0	0	0	0
8	0,0287	0,0323	0,0301	0,0249	0,0199	0,0152	0,0111	0,0080	0,0058	0,0040	0,0019	0,0009	0,0004	0,0002	0	0	0	0	0	0
9	0,0264	0,0286	0,0256	0,0200	0,0149	0,0106	0,0074	0,0050	0,0034	0,0022	0,0010	0,0004	0,0002	0	0	0	0	0	0	0
10	0,0244	0,0254	0,0212	0,0159	0,0112	0,0075	0,0049	0,0032	0,0020	0,0012	0,0006	0,0002	0	0	0	0	0	0	0	0
11	0,0225	0,0225	0,0178	0,0126	0,0083	0,0054	0,0032	0,0021	0,0013	0,0007	0,0002	0	0	0	0	0	0	0	0	0
13	0,0196	0,0179	0,0125	0,0080	0,0047	0,0027	0,0015	0,0009	0,0004	0,0002	0	0	0	0	0	0	0	0	0	0
15	0,0172	0,0147	0,0089	0,0050	0,0026	0,0010	0,0007	0,0004	0,0001	0	0	0	0	0	0	0	0	0	0	0
17	0,0151	0,0113	0,0061	0,0032	0,0015	0,0007	0,0003	0,0002	0	0	0	0	0	0	0	0	0	0	0	0
19	0,0133	0,0089	0,0044	0,0020	0,0008	0,0003	0,0001	0	0	0	0	0	0	0	0	0	0	0	0	0
21	0,0119	0,0071	0,0031	0,0013	0,0005	0,0002	0	0	0	0	0	0	0	0	0	0	0	0	0	0
23	0,0105	0,0056	0,0022	0,0009	0,0003	0,0001	0	0	0	0	0	0	0	0	0	0	0	0	0	0
25	0,0094	0,0044	0,0015	0,0005	0,0002	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27	0,0084	0,0034	0,0011	0,0003	0,0001	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29	0,0075	0,0027	0,0008	0,0002	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
31	0,0065	0,0022	0,0006	0,0002	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
33	0,0059	0,0017	0,0004	0,0001	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
35	0,0052	0,0015	0,0003	0,0001	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
37	0,0047	0,0011	0,0002	0,0001	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
39	0,0042	0,0008	0,0001	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
41	0,0037	0,0006	0,0001	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
46	0,0028	0,0004	0,0001	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
50	0,0020	0,0002	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

TABLE 4. The Variation of the Coefficients B_{i-m} for the Integral-Mean Temperature of the Sphere as a Function of the Computation Interval ΔFo and the Parameter $(i-m)$

$i-m$	ΔFo																			
	0,005	0,010	0,015	0,020	0,025	0,030	0,035	0,040	0,045	0,050	0,06	0,07	0,08	0,09	0,10	0,12	0,14	0,16	0,18	0,20
0	0,1521	0,2107	0,2539	0,2891	0,3193	0,3459	0,3697	0,3913	0,4112	0,4296	0,4627	0,4921	0,5183	0,5420	0,5636	0,6017	0,6344	0,6627	0,6875	0,7094
1	0,1171	0,1569	0,1840	0,2044	0,2206	0,2338	0,2448	0,2539	0,2616	0,2680	0,2779	0,2846	0,2889	0,2910	0,2917	0,2890	0,2827	0,2742	0,2644	0,2537
2	0,0710	0,0917	0,1040	0,1121	0,1174	0,1208	0,1226	0,1234	0,1231	0,1222	0,1185	0,1128	0,1060	0,0987	0,0910	0,0759	0,0620	0,0501	0,0400	0,0318
3	0,0546	0,0684	0,0756	0,0792	0,0806	0,0804	0,0792	0,0769	0,0741	0,0707	0,0631	0,0551	0,0475	0,0402	0,0337	0,0232	0,0156	0,0104	0,0067	0,0044
4	0,0450	0,0550	0,0590	0,0601	0,0594	0,0572	0,0542	0,0507	0,0467	0,0426	0,0347	0,0276	0,0214	0,0165	0,0125	0,0071	0,0039	0,0021	0,0012	0,0006
5	0,0387	0,0459	0,0480	0,0473	0,0450	0,0419	0,0390	0,0359	0,0319	0,0266	0,0192	0,0138	0,0098	0,0067	0,0046	0,0022	0,0010	0,0004	0	0
6	0,0340	0,0391	0,0398	0,0380	0,0348	0,0318	0,0267	0,0228	0,0191	0,0157	0,0106	0,0070	0,0044	0,0028	0,0017	0,0006	0,0003	0,0001	0	0
7	0,0302	0,0341	0,0335	0,0307	0,0269	0,0228	0,0190	0,0154	0,0122	0,0096	0,0059	0,0034	0,0021	0,0011	0,0006	0,0002	0	0	0	0
8	0,0273	0,0298	0,0283	0,0251	0,0210	0,0169	0,0133	0,0103	0,0078	0,0060	0,0032	0,0018	0,0008	0,0005	0,0002	0	0	0	0	0
9	0,0250	0,0265	0,0243	0,0205	0,0164	0,0127	0,0095	0,0069	0,0050	0,0036	0,0018	0,0008	0,0004	0,0002	0	0	0	0	0	0
10	0,0228	0,0235	0,0207	0,0167	0,0128	0,0093	0,0066	0,0047	0,0033	0,0022	0,0010	0,0005	0,0002	0	0	0	0	0	0	0
11	0,0211	0,0210	0,0179	0,0137	0,0100	0,0070	0,0048	0,0032	0,0021	0,0014	0,0005	0,0003	0,0001	0	0	0	0	0	0	0
13	0,0182	0,0170	0,0134	0,0092	0,0061	0,0039	0,0023	0,0018	0,0009	0,0005	0,0002	0,0001	0	0	0	0	0	0	0	0
15	0,0159	0,0138	0,0097	0,0063	0,0037	0,0021	0,0013	0,0007	0,0003	0,0002	0	0	0	0	0	0	0	0	0	0
17	0,0140	0,0112	0,0073	0,0042	0,0022	0,0012	0,0006	0,0003	0,0001	0	0	0	0	0	0	0	0	0	0	0
19	0,0124	0,0093	0,0054	0,0028	0,0013	0,0006	0,0002	0,0001	0	0	0	0	0	0	0	0	0	0	0	0
21	0,0111	0,0076	0,0040	0,0019	0,0008	0,0004	0,0001	0	0	0	0	0	0	0	0	0	0	0	0	0
23	0,0099	0,0062	0,0030	0,0013	0,0006	0,0002	0,0000	0	0	0	0	0	0	0	0	0	0	0	0	0
25	0,0090	0,0051	0,0022	0,0007	0,0003	0,0001	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27	0,0081	0,0042	0,0017	0,0005	0,0002	0,0001	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29	0,0072	0,0034	0,0012	0,0003	0,0001	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
31	0,0065	0,0028	0,0007	0,0002	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
33	0,0059	0,0023	0,0005	0,0001	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
35	0,0053	0,0019	0,0004	0,0001	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
37	0,0049	0,0015	0,0003	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
39	0,0044	0,0014	0,0002	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
46	0,0031	0,0010	0,0001	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
50	0,0025	0,0004	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

$i-m$	ΔFo							
	0,25	0,3	0,4	0,5	0,6	0,8	1,0	
0	0,7542	0,7884	0,8363	0,8892	0,9166	0,9333	0,9333	
1	0,2276	0,2031	0,1608	0,1105	0,0833	0,0656	0,0656	
2	0,0174	0,0078	0,0027	0,0003	0,0001	0	0	
3	0,0017	0,0005	0,0002	0	0	0	0	
4	0,0001	0	0	0	0	0	0	
5	0	0	0	0	0	0	0	

The problem of the determination of the heating of the cylinder and the sphere for a surface temperature variable in time can be solved on the basis of the relation (12) by applying Duhamel's theorem. Thus, if the entire thermal process is decomposed into equal time intervals in each of which the initial temperature is given as a linear function, i.e.,

$$t_w = t_w^{m-1} + \frac{t_w^m - t_w^{m-1}}{\Delta\tau} (\tau - \tau_{m-1}),$$

then (the temperature at the junction points of the computation intervals does not vary step-wise) the increase of the temperature at an arbitrary point of the cylinder (sphere), and of their integral-mean temperature is equal to:

$$\begin{aligned} t^1 &= t_w^1 B_0 \text{ at the end of the first,} \\ t^2 &= t_w^1 B_1 + t_w^2 B_0 \text{ at the end of the second,} \\ &\dots \dots \dots \\ t^i &= \sum_{m=1}^i t_w^m B_{i-m} \end{aligned} \tag{3}$$

at the end of the i -th time interval. Here

$$\begin{aligned} B_0 &= \sum_{n=1}^{\infty} A_n \left(1 - \frac{1}{\Delta Fo \mu_n^2} + \frac{1}{\Delta Fo \mu_n^2} e^{-\mu_n^2 \Delta Fo} \right); \\ B_{1,2,\dots,(i-1)} &= \sum_{n=1}^{\infty} \frac{A_n}{\Delta Fo \mu_n^2} [e^{-\mu_n^2 (i-m-1) \Delta Fo} - 2e^{-\mu_n^2 (i-m) \Delta Fo} + e^{-\mu_n^2 (i-m+1) \Delta Fo}]; \\ A_n &= \frac{4}{r \mu_n^2} \frac{J_1(\mu_n \bar{r})}{J_1(\mu_n)} \end{aligned}$$

for the integral-mean temperature of the cylinder of radius \bar{r} ;

$$A_n = 6(-1)^{n+1} \left(\frac{\sin \mu_n \bar{r}}{\mu_n \bar{r}} - \frac{\bar{r} \cos \mu_n \bar{r}}{\mu_n^2} \right)$$

for the integral-mean temperature of the sphere of radius \bar{r} ; the expressions of A_n for the temperature at the point of radius \bar{r} are given as clarifications to the formula (2).

The coefficients B_{i-m} , necessary for the determination of the center temperature and of the integral-mean temperature over the volume of the entire cylinder and sphere, we have computed for different values of the computation intervals ΔFo and their values for $(i-m) = 0-50$ are given in Tables 1-4, which allow the determination of the thermal stresses at the surfaces and in the centers of the cylinder and the sphere.

The results obtained by the given method coincide with the results obtained on the basis of the exact analytic solution of the heat conduction equations in the case of constant boundary conditions of the third kind.

In conclusion, it should be noted that the suggested method can be extended also to bodies of other form.

NOTATION

$\bar{r} = r/R$	is the relative coordinate;
α	is the coefficient of linear expansion;
E	is the modulus of elasticity;
ν	is Poisson's ratio;
τ	is the time;
a	is the specific thermal diffusivity;
$Fo = a\tau/R^2$;	
$\Delta Fo = a\Delta\tau/R^2$;	
$t(\bar{r})$	is the temperature as a function of the radius;
$t(0)$	is the temperature of the center;
t_w	is the surface temperature;
$\bar{t}(1), \bar{t}(\bar{r})$	are the integral-mean temperatures defined as $\bar{t}(k) = 2/k^2 \int_0^k t(\bar{r})\bar{r}d\bar{r}$ for

the cylinder and $\bar{t}(k) = 3/k^3 \int_0^k \bar{t}(\bar{r})\bar{r}^2 d\bar{r}$ for the sphere;

J_0 is the zero order Bessel function of the first kind;
 J_1 is the first order Bessel function of the first kind.

LITERATURE CITED

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